# A Mo(IV) Monophosphate, BaMo(PO<sub>4</sub>)<sub>2</sub>, with the Yavapaiite Layer Structure

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A new molybdenum monophosphate BaMo(PO<sub>4</sub>)<sub>2</sub> with the yavapailte structure has been synthesized and its structure was determined from a single crystal. This is the first phase of this family characterized by a reduced oxidation state of the transition element, i.e., Mo(IV). This layer monophosphate that crystallizes in the C2/m space group with a=8.211(1), b=5.2757(6), c=7.816(2) Å,  $\beta=94.778(1)^\circ$  exhibits close relationships with the tridimensional framework of  $\beta$ -cristoballite,  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub>, and CSMoOP<sub>2</sub>O<sub>7</sub>. © 1995 Academic Press, Inc.

### INTRODUCTION

The recent investigations of transition element phosphates have shown the possibility to synthesize numerous compounds in which the transition metal exhibits a reduced oxidation state. This is particularly the case of the molybdenophosphates of the systems A-Mo-P-O with A=Na, K, Rb,Cs, for which original mixed frameworks involving either Mo(V), Mo(IV), Mo(III), or mixed valencies of molybdenum have been isolated (see for instance for a review Ref. 1). Contrary to the alkaline phosphates, alkaline earth phosphates and especially barium molybdenophosphates have not been extensively studied up to date. The only barium compounds that have been isolated are the  $\text{BaMo}_2\text{P}_3\text{O}_{12}$  (2),  $\text{BaMo}_2\text{P}_4\text{O}_{14}$  (3),  $\text{BaMo}_2\text{P}_4\text{O}_{16}$  (4), and  $\text{BaMo}_4\text{P}_2\text{O}_{16}$  (5).

For this reason, the system Ba-Mo(IV)-P-O has been reinvestigated. This paper reports on the synthesis and crystal structure of a new monophosphate BaMo(PO<sub>4</sub>)<sub>2</sub> that exhibits the layered structure of the monoclinic aluns of the yavapaiite type (6, 7), also described for the phosphotitanate BaTi(PO<sub>4</sub>)<sub>2</sub>, by Masse and Durif (8). Structural relationships between the layer structure of yavapaiite and the tridimensional framework of  $\beta$ -cristoballite, nasicon, and of the phosphates  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub> (9) and CsMoOP<sub>2</sub>O<sub>7</sub> (10) are also studied.

# **SYNTHESIS**

The growth of single crystals of BaMo(PO<sub>4</sub>)<sub>2</sub> was performed in two steps starting from a mixture of nominal composition Ba<sub>3</sub>Mo<sub>4</sub>P<sub>6</sub>O<sub>24</sub>. First an adequate mixture of BaCO<sub>3</sub>,  $(NH_4)_2HPO_4$  and MoO<sub>3</sub> was heated at 973 K in a platinum crucible to eliminate CO<sub>2</sub>, H<sub>2</sub>O, and NH<sub>3</sub>. In the second step, the appropriate amount of molybdenum (1 mole) was added and the finely ground product sealed in an evacuated ampoule was heated up to 1173 K for 12 h and then quenched to room temperature.

Two sorts of crystals were extracted from the resulting product: mauve crystals and yellow crystals; the microprobe analysis of the first kind of crystals confirmed the composition BaMo(PO<sub>4</sub>)<sub>2</sub> deduced from the structure determination. The microprobe analysis of the yellow crystals revealed a new molybdenum phosphate involving barium but unfortunately the poor quality of the crystals did not allow their structure to be determined up to now. Subsequently a reaction to prepare pure powder BaMo(PO<sub>4</sub>)<sub>2</sub> was carried out at 1173 K for 12 hr, quenching the sample to room temperature. The powder X ray diffraction pattern (Table 1) of this new phosphate was indexed in a monoclinic cell (Table 2) in agreement with the parameters obtained from the single-crystal X ray study.

# STRUCTURE DETERMINATION

A mauve crystal with dimensions  $0.071 \times 0.038 \times 0.038$  mm was selected for the structure determination. The cell parameters reported in Table 2 were determined and refined by diffractometric techniques at 294 K with a least squares refinement based upon 25 reflections with  $18^{\circ} \le \theta \le 22^{\circ}$ . The data were collected on a CAD4 Enraf-Nonius diffractometer with the data collection parameters of Table 2. The reflections were corrected for Lorentz, polarization, and absorption effects. The systematic absences

TABLE 1 X Ray Powder Diffraction Data of BaMo(PO<sub>4</sub>)<sub>2</sub>

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1 1 0       4.437       4.434       89         2 0 0       4.096       4.091       77         3 0 2       3.900       3.894       34         4 1 1 1       3.775       3.781       44         2 0 1       3.511       3.504       10         1 1 2       2.998       2.994       100         2 0 2       2.948       2.946       11         1 1 2       2.863       2.863       58         2 0 2       2.712       2.710       14         3 2 0 2       2.640       2.638       54         4 0 0 3       2.597       2.596       6         5 1 0 2       2.272       2.279       3         3 1 1 2 2.266       1       2.266       1         2 2 0 2.220       2.217       11         3 1 2 2.158       2.184       27         2 2 1 2 2.185       2.184       27         2 2 2 1 2.185       2.199       2.129         2 0 3 1 .992       8       1.992         3 1 2 1.993       1.992       8         2 2 2 1 1.896       1.896       24         4 0 0 2 1.876       1.876       8         3 1 3 1 83	h —	k	<i>!</i> 	d <sub>obs</sub> (Å)	d <sub>cale</sub> (Å)	
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2       2       2       1.966       1.965       24         0       0       4       1.948       1.947       10         2       2       2       1.892       1.890       20         4       0       2       1.876       1.876       8         3       1       3       1.838       1.840       4         4       2       0       4       1.819       1.818       19         1       1       4       1.755       1.754       25         4       0       2       1.720       1.719       16         4       2       0       1.616       1.616       2         1       3       2       1.583       1.583       20         0       2       4       1.564       1.566       19         1       1       3       2       1.563       1.563         1       3       2       1.529       1.529       11         1       3       2       1.497       1.498       11         2       2       4       2       2       4       1.497	3	1				
1     1     4     1.755     1.754     25       4     0     2     1.752     1.719     16       1     3     0     1.720     1.719     16       4     2     0     1.616     1.616     2       1     3     2     1.583     1.583     20       0     2     4     1.564     1.566     19       5     1     0     1.563       1     3     2     1.563       4     2     2     1.529     1.529     11       2     0     5     1.497     1.498     11       2     2     4     1.497     1.497	2		2			
1     1     4     1.755     1.754     25       4     0     2     1.752     1.719     16       1     3     0     1.720     1.719     16       4     2     0     1.616     1.616     2       1     3     2     1.583     1.583     20       0     2     4     1.564     1.566     19       5     1     0     1.563       1     3     2     1.563       4     2     2     1.529     1.529     11       2     0     5     1.497     1.498     11       2     2     4     1.497     1.497	0		4			
1     1     4     1.755     1.754     25       4     0     2     1.752     1.719     16       1     3     0     1.720     1.719     16       4     2     0     1.616     1.616     2       1     3     2     1.583     1.583     20       0     2     4     1.564     1.566     19       5     1     0     1.563       1     3     2     1.563       4     2     2     1.529     1.529     11       2     0     5     1.497     1.498     11       2     2     4     1.497     1.497	2		2			
1     1     4     1.755     1.754     25       4     0     2     1.752     1.719     16       1     3     0     1.720     1.719     16       4     2     0     1.616     1.616     2       1     3     2     1.583     1.583     20       0     2     4     1.564     1.566     19       5     1     0     1.563       1     3     2     1.563       4     2     2     1.529     1.529     11       2     0     5     1.497     1.498     11       2     2     4     1.497     1.497	4		2			
1     1     4     1.755     1.754     25       4     0     2     1.752     1.719     16       1     3     0     1.720     1.719     16       4     2     0     1.616     1.616     2       1     3     2     1.583     1.583     20       0     2     4     1.564     1.566     19       5     1     0     1.563       1     3     2     1.563       4     2     2     1.529     1.529     11       2     0     5     1.497     1.498     11       2     2     4     1.497     1.497	3		3			
1     1     4     1.755     1.754     25       4     0     2     1.752     1.719     16       1     3     0     1.720     1.719     16       4     2     0     1.616     1.616     2       1     3     2     1.583     1.583     20       0     2     4     1.564     1.566     19       5     1     0     1.563       1     3     2     1.563       4     2     2     1.529     1.529     11       2     0     5     1.497     1.498     11       2     2     4     1.497     1.497	2	0	4			19
4     0     2     1.752       1     3     0     1.720     1.719     16       4     2     0     1.616     1.616     2       1     3     \frac{7}{2}     1.583     1.583     20       0     2     4     1.564     1.566     19       5     1     0     1.563       1     3     2     1.563       4     2     \frac{7}{2}     1.529     1.529     11       2     0     \frac{7}{5}     1.497     1.498     11       2     2     \frac{7}{4}     1.497	1	1				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4	0				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1			1.720		16
1     3     \overline{2}     1.583     20       0     2     4     1.564     1.566     19       5     1     0     1.563       1     3     2     1.563       4     2     \overline{2}     1.529     1.529       2     0     \overline{5}     1.497     1.498     11       2     2     \overline{4}     1.497	4					
0     2     4     1.564     1.566     19       5     1     0     1.563       1     3     2     1.563       4     2     \overline{2}     1.529     1.529       2     0     \overline{5}     1.497     1.498     11       2     2     \overline{4}     1.497	i					
5     1     0     1.563       1     3     2     1.563       4     2     \overline{2}     1.529     1.529       2     0     \overline{5}     1.497     1.498     11       2     2     \overline{4}     1.497	Ô	2	4			
1     3     2     1.563       4     2     \overline{2}\$     1.529     1.529     11       2     0     \overline{5}\$     1.497     1.498     11       2     2     \overline{4}\$     1.497	5			• ,		• •
	1					
	4		$\frac{2}{2}$	1.529		11
	2		3			
	2		4	*****		- 1
	3			1.478		24
	_			1,70	1,470	

h + k = 2n + 1 for all hkl are consistent with the C2, Cm, or C2/m space group. The atoms were located by the heavy atom method and successfully refined in the centrosymmetric space group C2/m. The positional and thermal parameters for BaMo(PO<sub>4</sub>)<sub>2</sub> listed in Table 3 lead to the factors R = 0.030 and  $R_w = 0.036$ .

### RESULTS AND DISCUSSION

The projection of the structure of BaMo(PO<sub>4</sub>)<sub>2</sub> onto the (010) plane (Fig. 1) shows the layered character previously found for the alun sulfates (6, 7). It consists of very simple  $[MoP_2O_8]_{\infty}$  layers built up from corner-sharing PO<sub>4</sub> tetrahedra and  $MoO_6$  octahedra, and interleaved with barium

TABLE 2
Summary of Crystal Data Intensity, Measurements and Structure Refinement Parameters for BaMo(PO<sub>4</sub>)<sub>2</sub>

<u>-</u> ۱	Crystal data				
1.	Space group	C2/m			
	Cell dimensions	a = 8.211(1)  Å			
	Cen amjorisjons	$b = 5.2757(6)$ $\beta = 94.77(1)^{\circ}$			
		c = 7.816(2)			
	Volume (Å) <sup>3</sup>	337.4(2)			
	Z	2			
	$\rho_{\rm calc}$ (gcm <sup>3</sup> )	4.17			
2.	Intensity measurements				
	$\lambda(MoK\alpha)$	0.71073			
	Scan mode	ω			
	Scan width (°)	$1.3 + 0.35 \tan \theta$			
	Slit aperture (mm)	$1.4 + \tan \theta$			
	Max $\theta$ (°)	45			
	Standard reflections	3 measured every 3600 sec			
	Measured reflections	1554			
	Reflections with $I > 3\sigma$	801			
	$\mu(\text{mm}^{-1})$	8.09			
3.	Structure solution and refinement				
	Parameters refined	37			
	Agreement factors	$R = 0.030$ $R_{\rm w} = 0.036$			
	Weighting scheme	$w = f(\sin \theta/\lambda)$			
	Δ/σ max	< 0.004			
_	A/O Mux				

cations. Note that each PO<sub>4</sub> tetrahedron exhibits one free apex pointing out of the layer.

Each MoO<sub>6</sub> octahedron shares its six apices with PO<sub>4</sub> tetrahedra as shown from the projection of one layer onto the (001) plane (Fig. 2). Reciprocally, each PO<sub>4</sub> tetrahedron is linked to three MoO<sub>6</sub> octahedra. As a result each PO<sub>4</sub> tetrahedron exhibits three identical P-O distances corresponding to the P-O-Mo bonds, i.e., to O(1) and O(2), and a shorter P-O bond corresponding to the free apex O(3) (Table 4). The Mo-O distances of the MoO<sub>6</sub> octahedron (Table 4) are similar to those observed for other Mo(IV) monophosphates. Note however, that the geometry of the MoO<sub>6</sub> octahedron is very similar to that

TABLE 3
Positional Parameters and Their Estimated Standard Deviations

Atom	х	у	z	B(A2)
Ba	0.	0.	0.	1.309(6)
Mo	0.	0.	0.5	0.856(8)
P	0.1294(2)	0.5	0.2899(2)	0.88(2)
O(1)	0.0242(4)	0.2610(6)	0.3123(4)	1.29(4)
O(2)	0.2652(5)	0.5	0.4392(6)	1.21(6)
O(3)	0.1862(6)	0.5	0.1122(6)	1.65(7)

Note. Anisotropically refined atoms are given in the form of the isotropic equivalent displacement parameter defined as

$$B = (4/3) \sum_{i} \sum_{j} \vec{a}_{i} \cdot \vec{a}_{j} \beta_{ij}.$$

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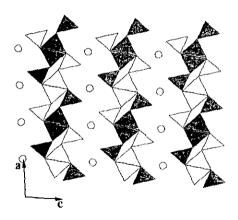


FIG. 1. Projection of the BaMo(PO<sub>4</sub>), structure along [010].

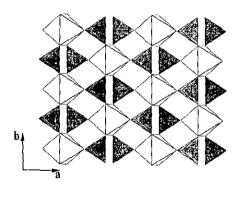


FIG. 2. Projection of a [MoP<sub>2</sub>O<sub>8</sub>]<sub>x</sub> layer onto the [001] plane.

of the FeO<sub>6</sub> octahedron in the mineral yavapaiite (7); one indeed observed in both cases a flattening of this polyhedron leading to two short Mo(Fe)-O bonds (1.947-1.954 Å) and four larger ones (2.00-2.034 Å).

The barium cation is linked to four O(1) atoms located within the  $[MoP_2O_8]_{\infty}$  layer and to two O(3) atoms corre-

sponding to the free apices of the PO<sub>4</sub> tetrahedra. Like potassium in the yavapaiite, barium exhibits an octahedral coordination. However, the BaO<sub>6</sub> octahedron, with six Ba-O distances ranging from 2.79 to 2.795 Å (Table 4), is remarkably regular (Fig. 3) compared to the KO<sub>6</sub> octahedron (2.826 to 2.860 Å). It appears as one of the most

TABLE 4
Distances (Å) and Angles (°) in the Polyhedra

Mo	O(1 <sup>i</sup> )	O(1)	O(1 <sup>ii</sup> )	O(1 <sup>iii</sup> )	O(2 <sup>iv</sup> )	O(2 <sup>v</sup> )
O(1 <sup>i</sup> )	2.034(3)	4.067(7)	2.754(7)	2.994(7)	2.846(5)	2.784(5)
O(1)	180	2.034(3)	2.994(7)	2.754(7)	2.784(5)	2.846(5)
$O(1^{ii})$	85.2(2)	94.8(2)	2.034(3)	4.067(7)	2.846(5)	2.784(5)
$O(1^{iii})$	94.8(2)	85.2(2)	180	2.034(3)	2.784(5)	2.846(5)
$O(2^{iv})$	88.7(2)	91.3(1)	88.7(2)	91.3(2)	1.947(4)	3.894(7)
O(2 <sup>v</sup> )	91.3(2)	88.7(2)	91.3(2)	88.7(2)	180	1.947(4)
P	O(1)	O(1 <sup>vi</sup> )	O(2)	O(3)		
O(1)	1.547(4)	2.522(7)	2.483(5)	2.480(5)	· <del></del>	
$O(1^{vi})$	109.2(3)	1.547(4)	2.483(5)	2.480(5)		
O(2)	106.8(2)	106.8(2)	1.546(5)	2.584(7)		
O(3)	108.9(2)	108.9(2)	116.0(3)	1.501(5)		
			$Ba-O(1^{vii}) = 2.795(4$	)		
			O(1) = 2.795(4)	5)		
			$O(1^{\hat{u}\hat{i}}) = 2.795(4$	)		
			$O(1^{viii}) = 2.795(4$	)		
			$O(3^{iv}) = 2.790(5)$			
			$O(3^{ix}) = 2.790(5)$	)		

## Symmetry code

- (i)  $-x_1 y_1 + z_2$
- (ii) -x, y, 1-z
- (iii) x, -y, x
- (iv) x = 1/2, y = 1/2, z
- (v) 1/2 x, 1/2 y, 1 z
- (vi) x, 1 y, z
- (vii) -x, -y, -z
- (viii) -x, y, -z
- (ix) 1/2 x, 1/2 y, -z

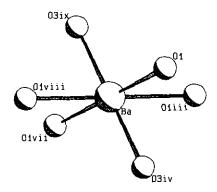


FIG. 3. The oxygen polyhedron around Ba.

regular octahedra encountered in the  $AM(XO_4)_2$  structures. Moreover, the next nearest oxygen neighbors are located at much larger distances (>3.5 Å), contrary to potassium in the yavapaiite structure that exhibits three additional neighbors at 3.12 Å.

Many compounds with the generic formulation  $AM(XO_4)_2$  with X = S, Se, Cr, Mo, W, and P have been synthesized up to date. Most of them exhibit a layer structure with close relationships that have lead to an interesting structural classification (11). In this classification the yavapaiite structure, and consequently  $BaMo(PO_4)_2$ , belongs to category II; i.e., it can be considered as the less distorted structure with respect to the highest symmetry  $P\overline{3}ml$  observed for the class I compounds. Thus the  $[MoP_2O_8]_\infty$  layers (Fig. 2) derive from the ideal trigonal layers (Fig. 4) of  $KAl(MoO_4)_2$  (12) by a rotation of the  $PO_4$  tetrahedra around axis located within the layer as already described (11).

The most interesting feature leads with the close relationships between the layer structure of the  $AM(XO_4)_2$  compounds and the tridimensional structures of  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub> (9) and consequently of  $\beta$ -cristoballite. Considering the view of the BaMo(PO<sub>4</sub>)<sub>2</sub> structure along b (Fig. 1), a tridimensional framework [MoP<sub>2</sub>O<sub>8</sub>]<sub> $\infty$ </sub> similar to that of  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub> (Fig. 5) can be obtained by translating two successive [MoP<sub>2</sub>O<sub>8</sub>]<sub> $\infty$ </sub> layers of ( $(\vec{a}/3) + (\vec{c}/5)$ ) with respect

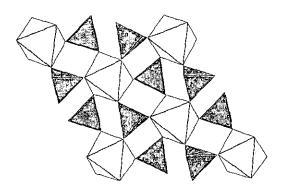


FIG. 4. The  $[TiP_2O_8]_{x}$  layer in  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub>.

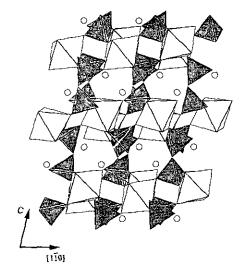


FIG. 5. The projection of the  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub> structure along [110] showing the octahedral layers and the P<sub>2</sub>O<sub>7</sub> layers.

to each other and by connecting the PO<sub>4</sub> tetrahedra of these two layers. In this way, the [MoP<sub>2</sub>O<sub>7</sub>]<sub>∞</sub> framework consists, like the [TiP<sub>2</sub>O<sub>7</sub>]<sub>x</sub> framework, of octahedral layers connected through layers of diphosphate groups. It results in distorted hexagonal tunnels with a disposition very similar to that of  $\beta$ -cristoballite (Fig. 6). In fact the BaMo(PO<sub>4</sub>)<sub>2</sub> structure differs mainly from the  $\alpha$ -NaTiP<sub>2</sub>O<sub>2</sub> structure by the distortion of the [MoP<sub>2</sub>O<sub>8</sub>]<sub>∞</sub> layers (Fig. 2). The  $\alpha$ -NaTiP<sub>2</sub>O<sub>2</sub> structure can indeed be described as the stacking of mixed [TiP<sub>2</sub>O<sub>8</sub>]<sub>x</sub> layers absolutely similar to the [AlMo<sub>2</sub>O<sub>8</sub>]<sub>∞</sub> (Fig. 4) encountered in the molybdate KAl(MoO<sub>4</sub>)<sub>2</sub> (12), i.e., built up from corner-sharing TiO<sub>6</sub> octahedra and PO<sub>4</sub> tetrahedra with the  $P\overline{3}1m$  symmetry. In summary, the KAl(MoO<sub>4</sub>)<sub>2</sub> layer structure (class I) derives from the  $\alpha$ -NaTiP<sub>2</sub>O<sub>2</sub> structure by a simple sharing mechanism at the level of the bridging oxygen of the P<sub>2</sub>O<sub>7</sub> groups leading to the formation of single MoO<sub>4</sub> tetrahedra (instead of MoO<sub>2</sub> groups), whereas in the BaMo(PO<sub>4</sub>)<sub>2</sub> structure (class II), the sharing mechanism at the level of

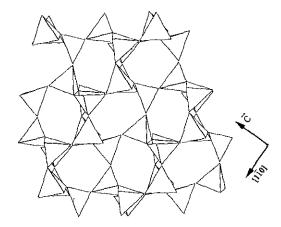


FIG. 6. The projection of the  $\beta$ -cristoballite structure along [110].

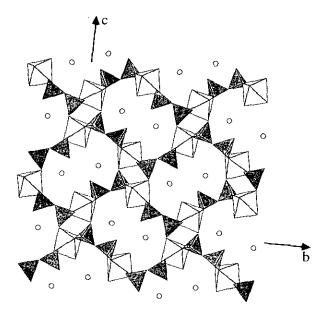


FIG. 7. Projection of the structure of CsMoP<sub>2</sub>O<sub>8</sub> along  $\vec{a}$ .

the bridging oxygen is followed by a distortion of the  $[MoP_2O_8]_{\infty}$  layers.

The close relationships that have been previously established between  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub> and  $\beta$ -cristoballite (9) make obvious the structural filiation between these different compounds. Let us indeed recall that the  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub> structure derives from the  $\beta$ -cristoballite structure by replacing one (111) layer of P<sub>2</sub>O<sub>7</sub> groups out of two by one layer of TiO<sub>6</sub> octahedron (compare Figs. 5 and 6).

The close relationships between the CsMoOP<sub>2</sub>O<sub>7</sub> (10) and  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub> (9) structures, which both consist of the stacking of similar layers of P<sub>2</sub>O<sub>7</sub> groups with layers of TiO<sub>6</sub> (or MoO<sub>6</sub>) octahedra, show that the layer structures

 $AM(XO_4)_2$  are also closely related to the tridimensional framework of CsMoOP<sub>2</sub>O<sub>7</sub> (Fig. 7). Nevertheless, it must be pointed out that in the latter, the P<sub>2</sub>O<sub>7</sub> groups exhibit a staggered configuration contrary to  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub> so that the orientations of the successive octahedral layers are different in the two structures.

In conclusion, the Mo(IV) monophosphate BaMo(PO<sub>4</sub>)<sub>2</sub> is the only one that involves a reduced oxidation state of the transition element among all the compounds  $AM(XO_4)_2$  related to the yavapaiite structure. This feature and the close relationships with the tridimensional structures of  $\beta$ -cristoballite and  $\alpha$ -NaTiP<sub>2</sub>O<sub>7</sub> open the route to research of other phosphates related to this family.

#### REFERENCES

- 1. R. C. Haushalter and L. A. Mundi, Chem. Mater. 4, 31 (1992).
- A. Leclaire, M. M. Borel, A. Grandin, and B. Raveau, Eur. J. Solid State Inorg. Chem. 26, 45 (1989).
- A. Leclaire, J. Chardon, M. M. Borel, A. Grandin, and B. Raveau, Z. Anorg. Allg. Chem. 617, 127 (1992).
- G. Costentin, M. M. Borel, A. Grandin, and B. Raveau, J. Solid State Chem. 89, 83 (1990).
- M. M. Borel, J. Chardon, A. Leclaire, A. Grandin, and B. Raveau, J. Solid State Chem. 112, 317 (1994).
- 6. C. O. Hutton, Am. Miner. 44, 1105 (1959).
- 7. E. J. Graeber and A. Rosenzweig, Am. Miner. 56, 1917 (1971).
- R. Masse and A. Durif, C.R. Acad. Sci. Paris, Sér. C 274, 1692 (1972).
- A. Leclaire, A. Benmoussa, M. M. Borel, A. Grandin, and B. Raveau, J. Solid State Chem. 72, 299 (1988).
- A. Guesdon, M. M. Borel, A. Grandin, A. Leclaire, and B. Raveau, J. Solid State Chem. 108, 46 (1993).
- S. Oyetola, A. Verbaere, Y. Piffard, and M. Tournoux, Eur. J. Solid State Inorg. Chem. 25, 259 (1988).
- 12. R. F. Klevtsova and P. V. Klevtsov, Kristallografiya 15, 953 (1970).